## Rheological Modelling of Metal-Polymer-Oxide Ceramics Composite

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## EXTENDED ABSTRACT

In the paper fracture of Al-Al<sub>2</sub>O<sub>3</sub>-Diamonds containing composite coating has been investigated by using rheological models for principal Hertzian contact of a sphere and a plate. Several requirements to the rheological models were formulated regarding adequate strain-deformation state.

Rheological model of the composite coating has been proposed and confirmed by in-suit experiments. The coating was presented as complex elastic-viscous-plastic rheological model and/or a rheological model from two elastic elements and one viscous element that is the Maxwells' model and an elastic element. Structural equation of an integral model is written as  $(H \parallel N \parallel St-V) - (H-N \parallel H)$ . If  $s > s_0$ , then rheological model of the former model may be described as

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}_0 + E_1 \boldsymbol{\varepsilon}_1 + \boldsymbol{\eta}_1 \, \frac{d\boldsymbol{\varepsilon}_1}{dt}.$$
 (1)

where  $s_0$  is ultimate strain;  $?_1$  is Young's modulus;  $?_1$  is coefficient of viscosity; e - deformation. If  $s > s_0$ , then rheological model of the later model is

$$\frac{d\sigma}{dt} + \frac{E_{22}}{\eta_2}\sigma = (E_{21} + E_{22})\frac{d\varepsilon_2}{dt} + \frac{E_{21}E_{22}}{\eta_2}\varepsilon_2$$
 (2)

where  $?_{21}$ ,  $?_{22}$  are Young's modules;  $?_2$  is coefficient of viscous element.

Under random loading rate integral rheological equation for the joined models will be as follows

$$\frac{\eta_1}{E_{22}} \frac{d^2 \sigma}{dt^2} + \left(\frac{E_1}{E_{22}} + \frac{\eta_1}{\eta_2} + \beta\right) \frac{d\sigma}{dt} + \frac{E_1 + E_{21}}{\eta_2} \sigma - \frac{E_{21}}{\eta_2} \sigma_0 = \beta\eta_1 \frac{d^2 \varepsilon}{dt^2} + \left(\frac{\eta_1}{\eta_2} E_{21} + \beta E_1\right) \frac{d\varepsilon}{dt} + \frac{E_1 E_{21}}{\eta_2} \varepsilon$$

The crystallographic and morphologic texture was characterized and the fracture resistance was measured, using fracture-mechanics. Examination of the composite coating shows a hardness value of 25 GPa (about 25% higher than alumina-based layer) and fracture resistance (about 50% higher than for single oxide ceramic layer) as compared to prior alumina-based coatings on a soft substrate.

Experiments revealed ultimate stresses and stress-deformation modes of the coating. Diamonds nanoparticles improve fracture resistance of alumina-based layer. It is also thought that the composite coatings will have higher thermal conductivity and thermal shock resistance than that of alumina-based layer. Such physical characteristics suggest a number of possible commercial applications for the composite coatings, particularly for wear-resistant and related applications. The higher hardness and toughness of the coatings make them very attractive as substitutes for alumina-based and other ceramic-based composite coatings in these applications.